

# CFRP Upper Wing Cover for Natural Laminar Flow

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Knowledge for Tomorrow



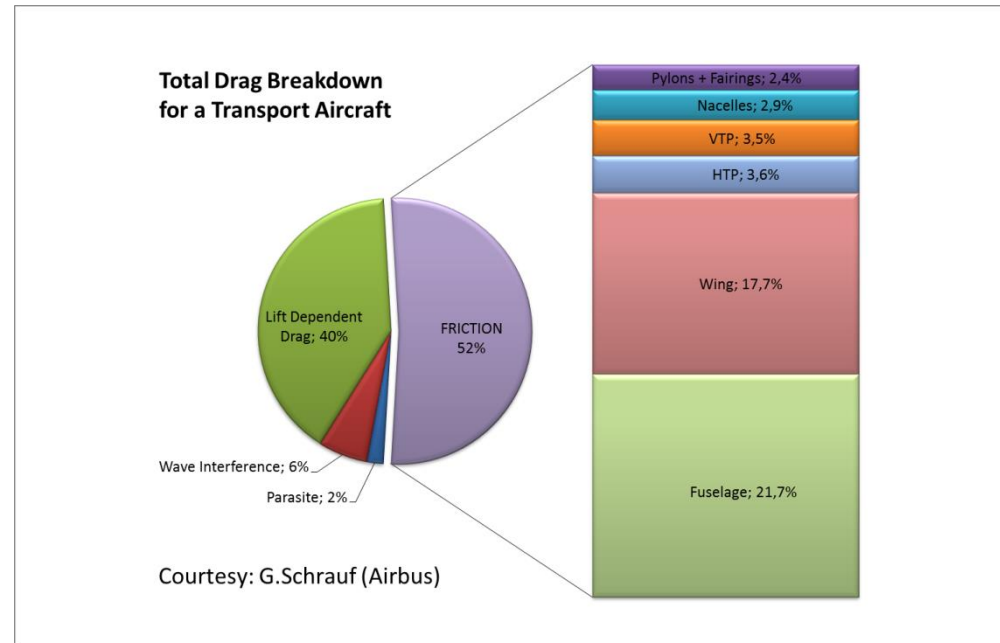
# Content

- Motivation: Why natural laminar flow?
- Structural Concept for NLF Upper Wing Cover
- Manufacturing Concept
- Process induced Deformations (PID)
- Load induced Deformations (LID), Sizing Process
- Manufacturing Process of integral Wing Upper Cover
- Optical Measurement
- Resulting Waviness from PID and LID
- Summary



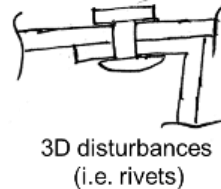
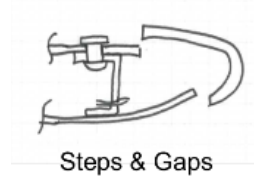
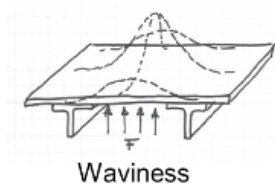
# Why laminar flow?

- Laminar Flow can reduce friction drag significantly!
- 5% to 8% Reduction of friction drag is possible for typical wing applications

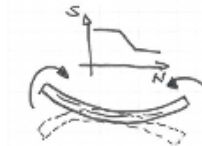


# Requirements for Laminar Wing

## Aerodynamic Requirements



## Structural Requirements



Aerodynamic requirements have to be achieved under typical production standards (high rate, low cost) to be beneficial on aircraft level!



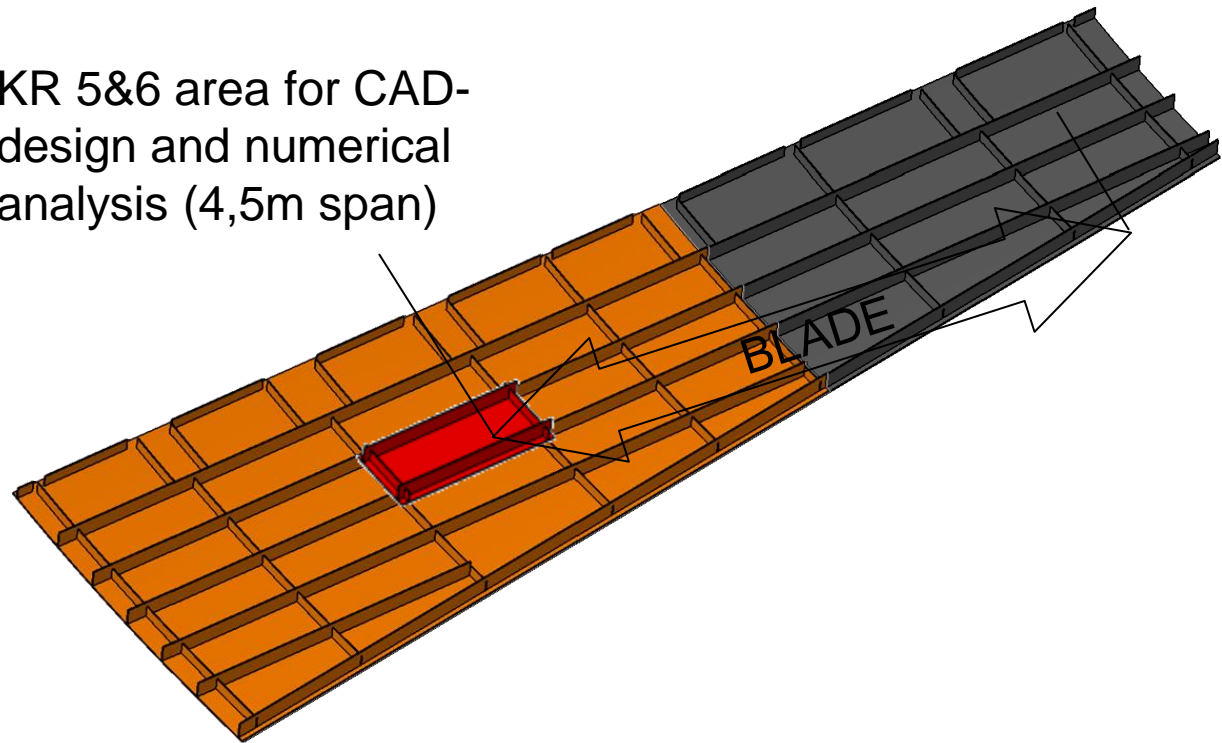
# Wing geometry & manufactured parts

NLF wing research configuration NLF13

LaWiPro Panel (1,0m x 0,6m)

LaWOp Panel (2,5m x 1,5m)

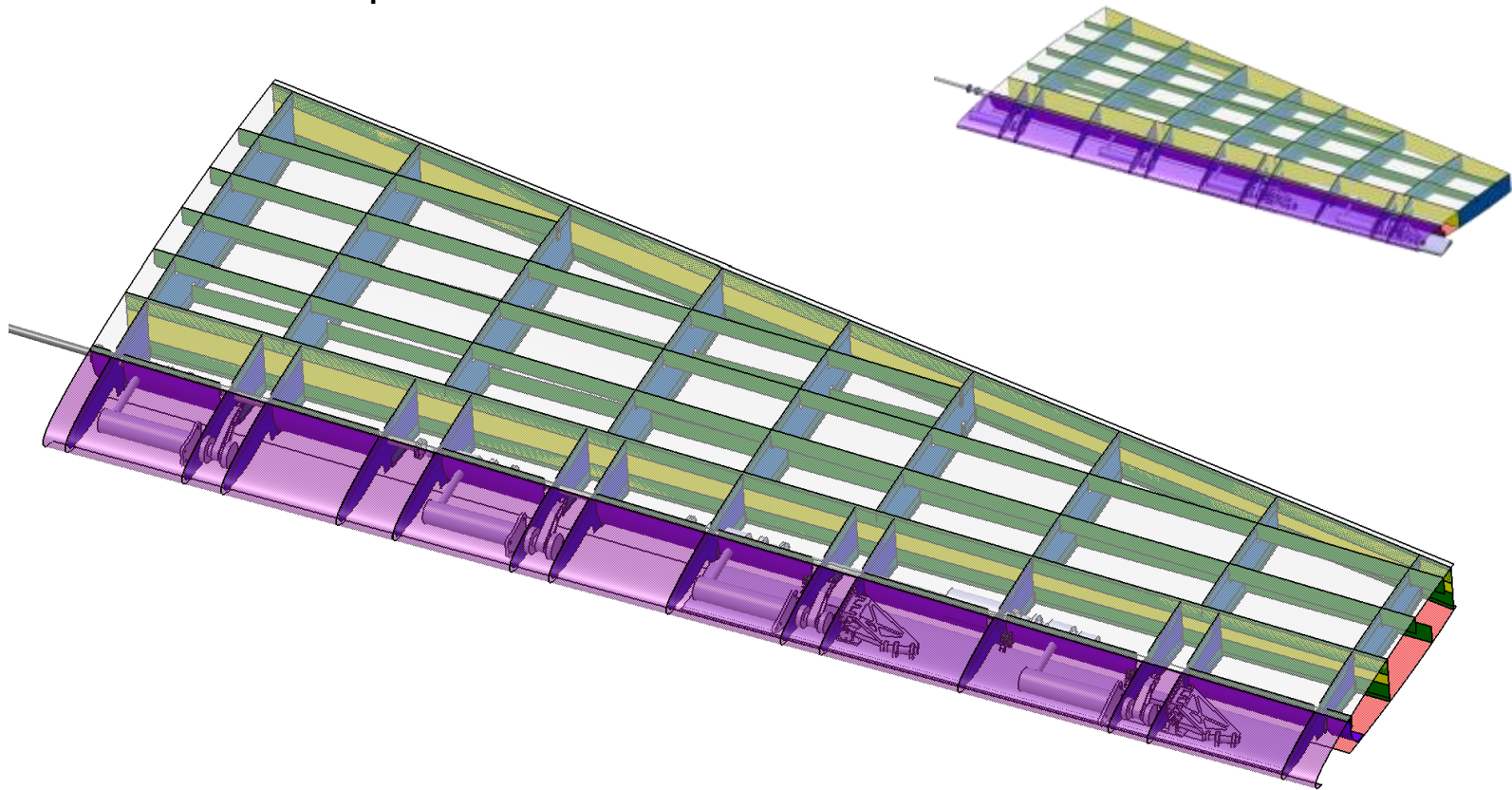
KR 5&6 area for CAD-design and numerical analysis (4,5m span)



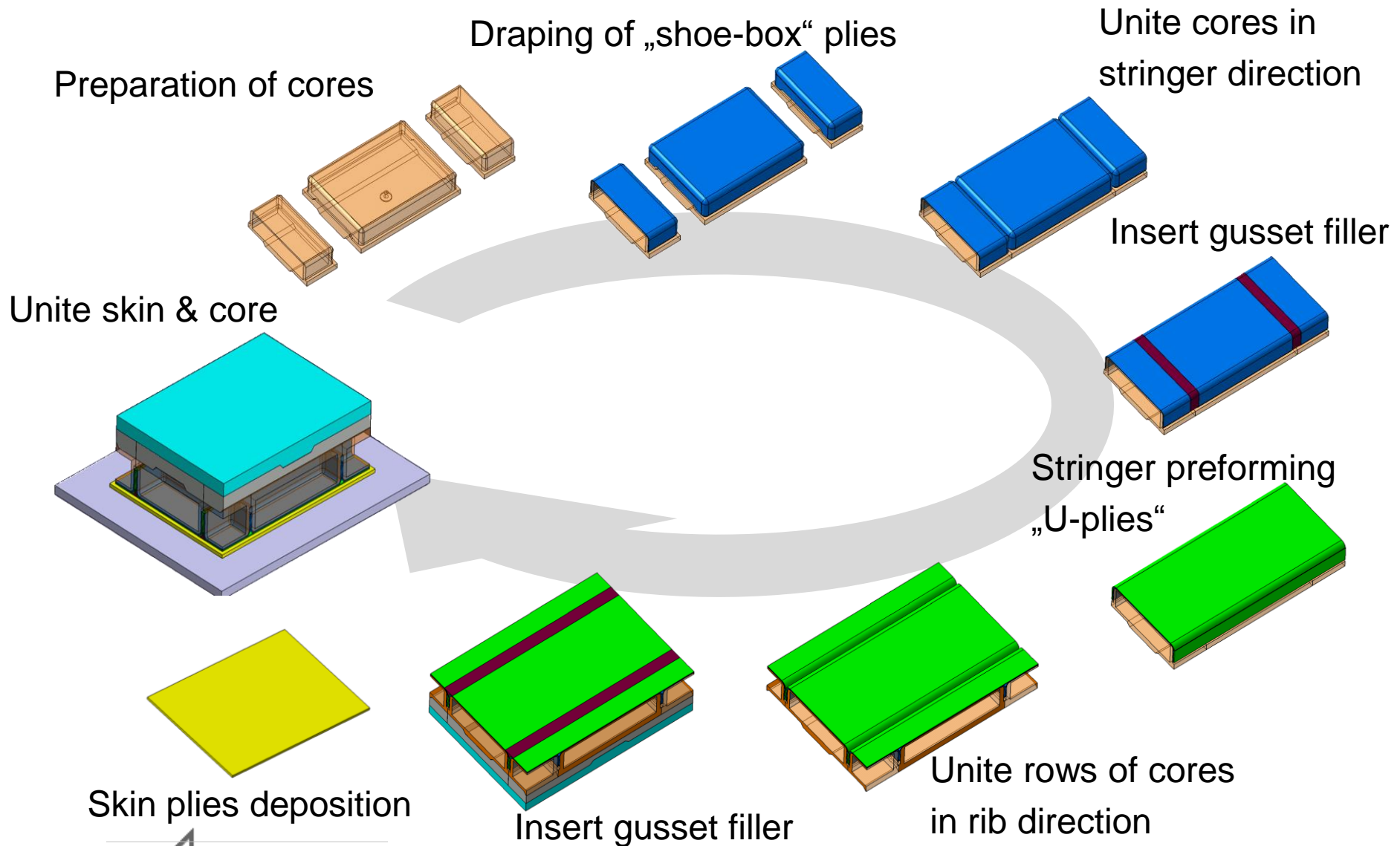


# Basic Concept – DLR V6

Final Basic Design: new rib positions in Leading Edge implemented  
ribs perpendicular to Front Spar

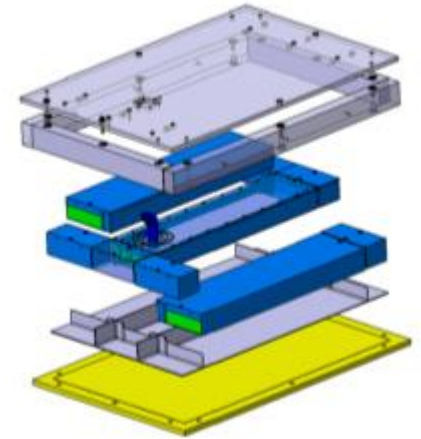


# Production Concept

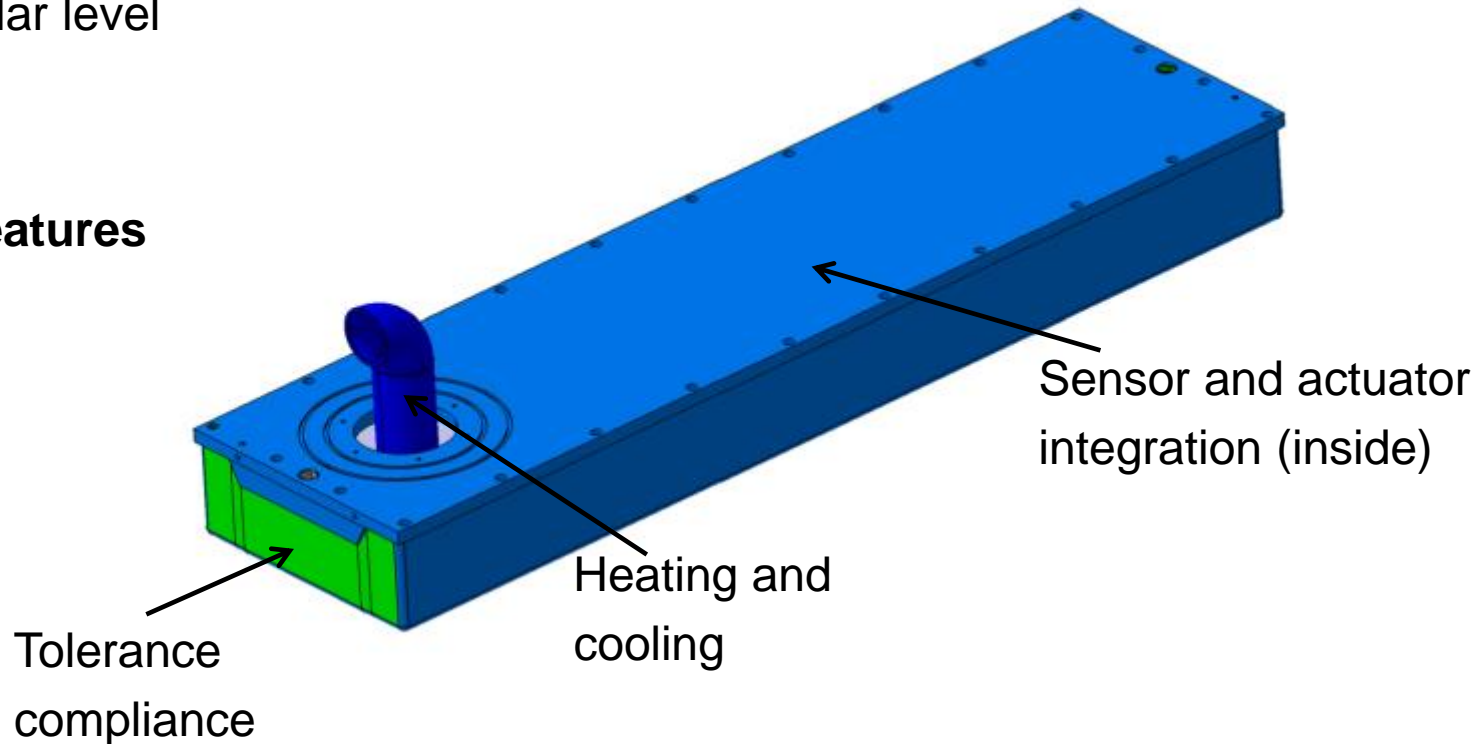


# Cellular Tooling Concept

- Moulding of the stiffeners is done by many similar elements/ cells
- Address all issues and challenges on a local/ cellular level

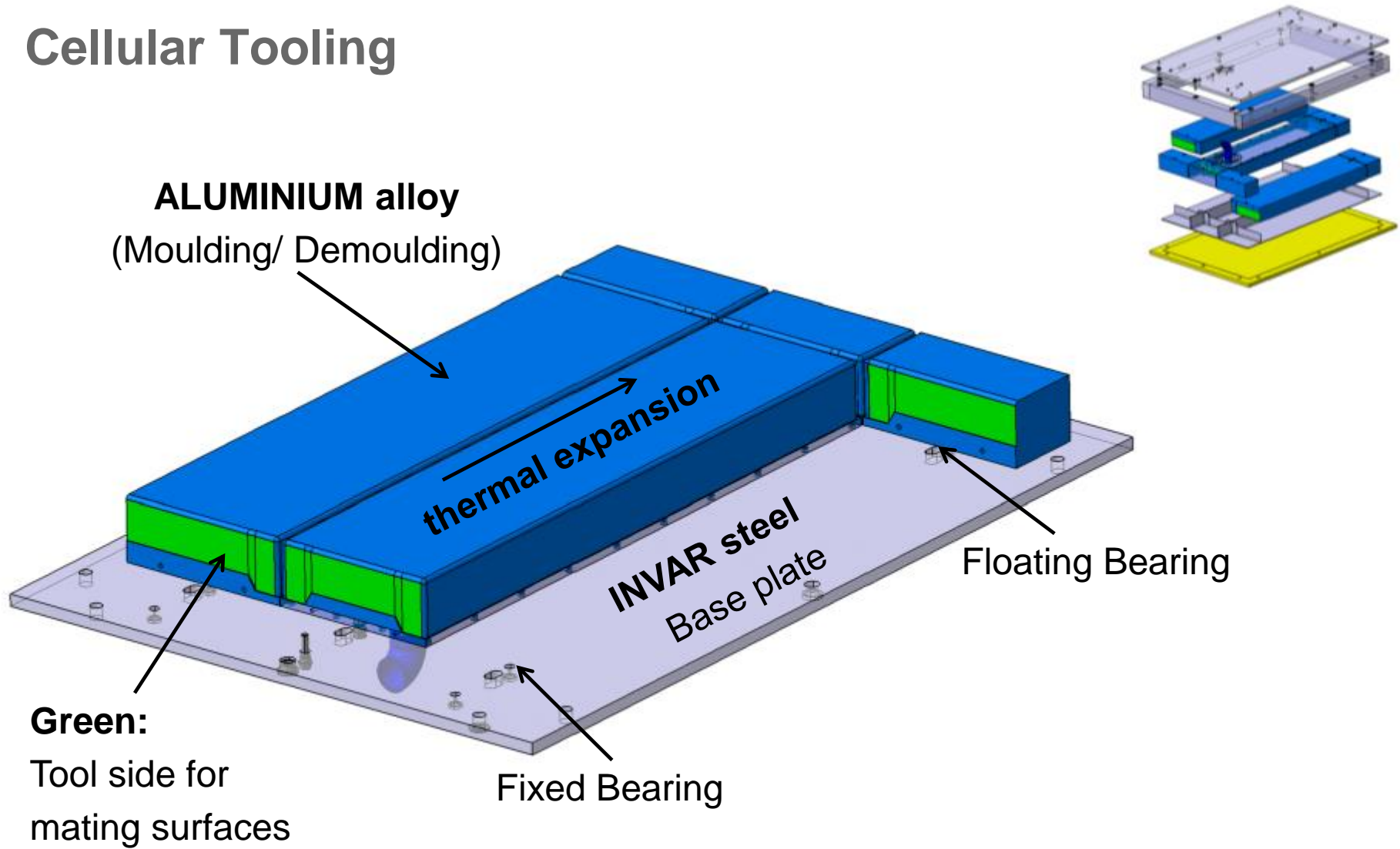


## Cell features

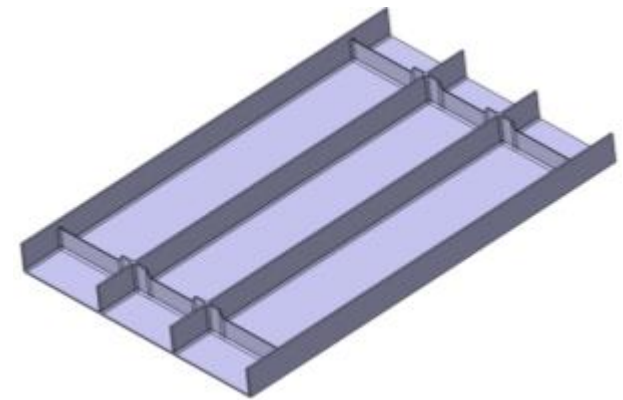
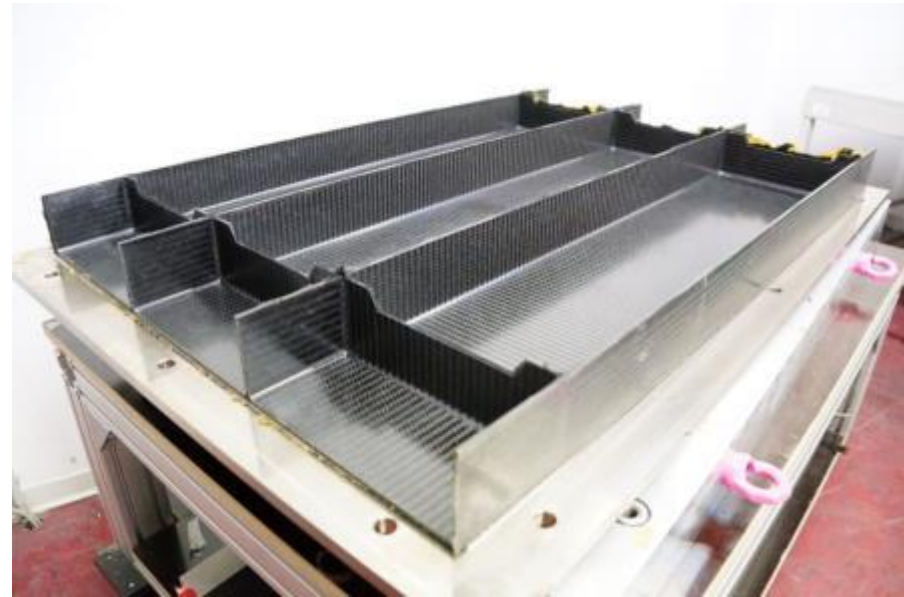
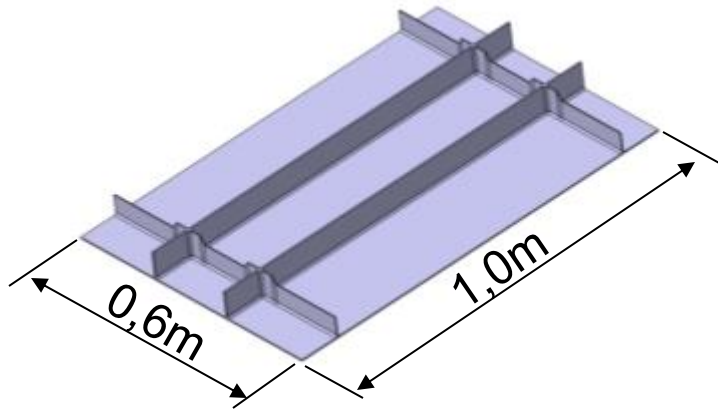




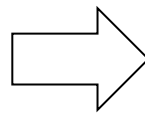
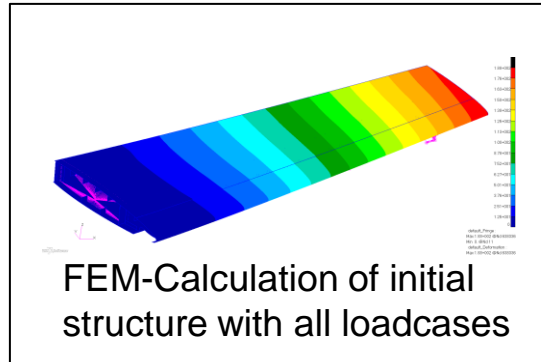
# Cellular Tooling



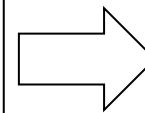
# Proof of Manufacturing Concept



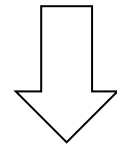
# Sizing of Wing Upper Cover



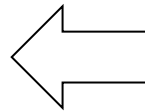
Identification of critical loadcase and sizing criteria



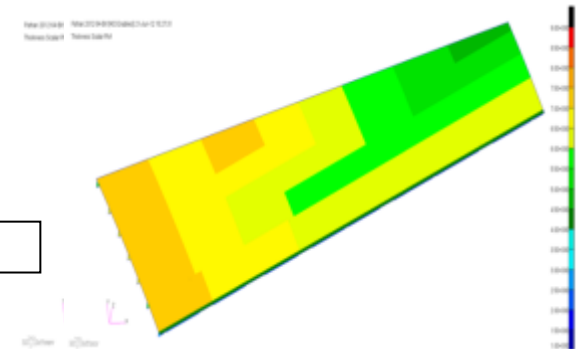
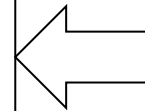
Structural sizing for critical loadcase and criteria



Layup sequence for wing upper cover and internal substructure



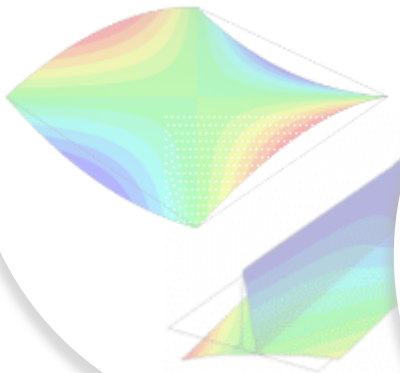
Checking dimensioning criterias up to convergence:  
Strength / Buckling /  
Damage Tolerance /  
Rivet Failure / Waviness



# Process induced Deformations (PID)

- Process distortions are driven by residual stresses
- Different inducing phenomena

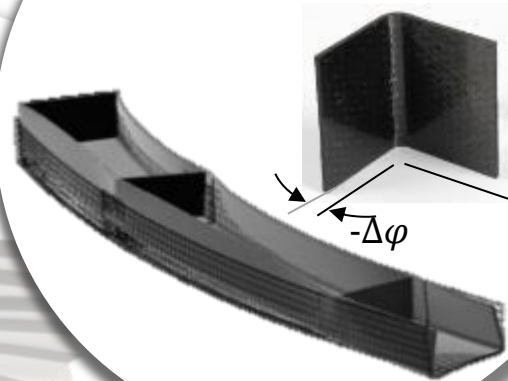
Layup asymmetry



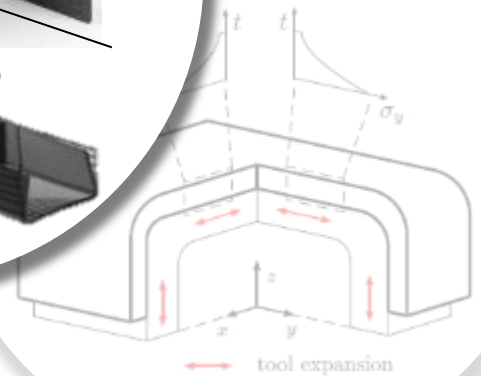
Warpage



Spring-In

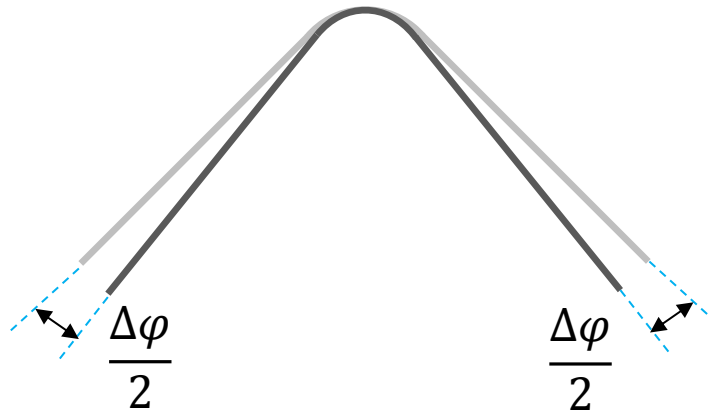


Interaction

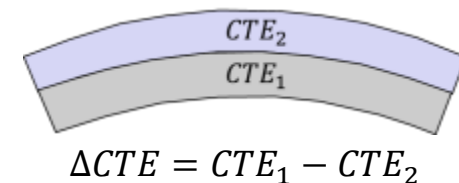
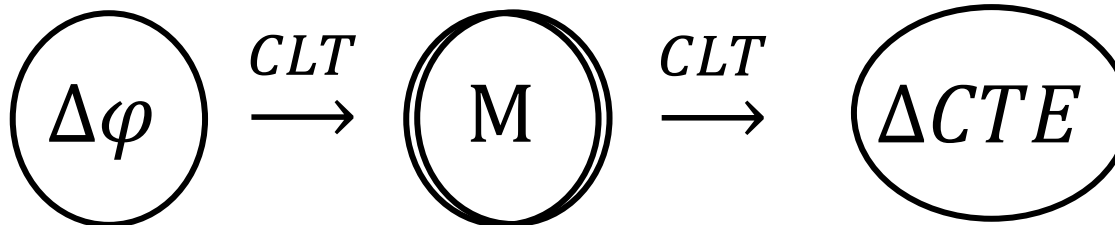
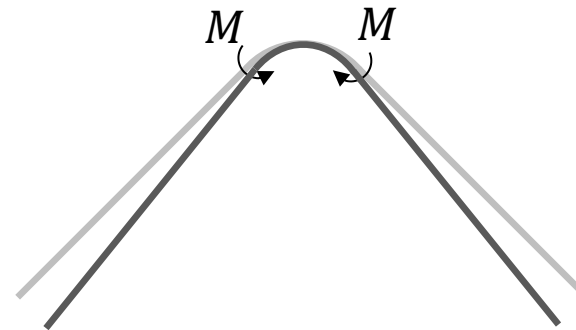


# Semi-numerical model approach

Specimen deformation



Corresponding model

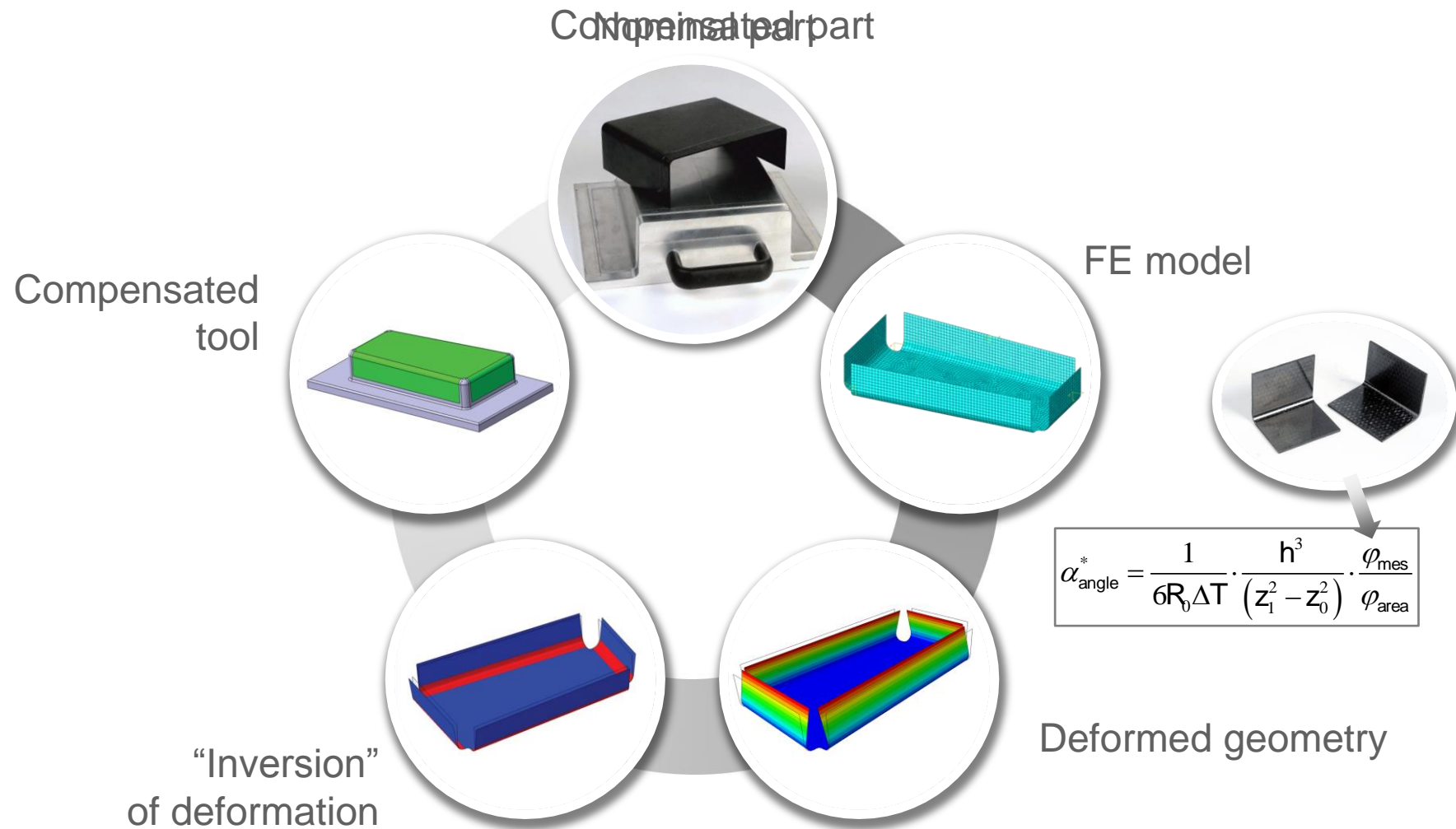


$$\begin{Bmatrix} \underline{\varepsilon}^0 \\ \underline{\kappa} \end{Bmatrix} = \begin{Bmatrix} \underline{A} & \underline{B} \\ \underline{B} & \underline{D} \end{Bmatrix}^{-1} \cdot \underline{M}^* \cdot \underline{N} \cdot \begin{Bmatrix} M_x^* \\ M_y^* \\ M_{xy}^* \end{Bmatrix} = \underline{\bar{Q}}_1 \cdot \Delta T \cdot \begin{Bmatrix} \alpha_x^* \\ \alpha_y^* \\ \alpha_{xy}^* \end{Bmatrix}_1 \cdot \frac{1}{2} (h_1^2 - h_0^2)$$





# Simulation of Process induced deformations



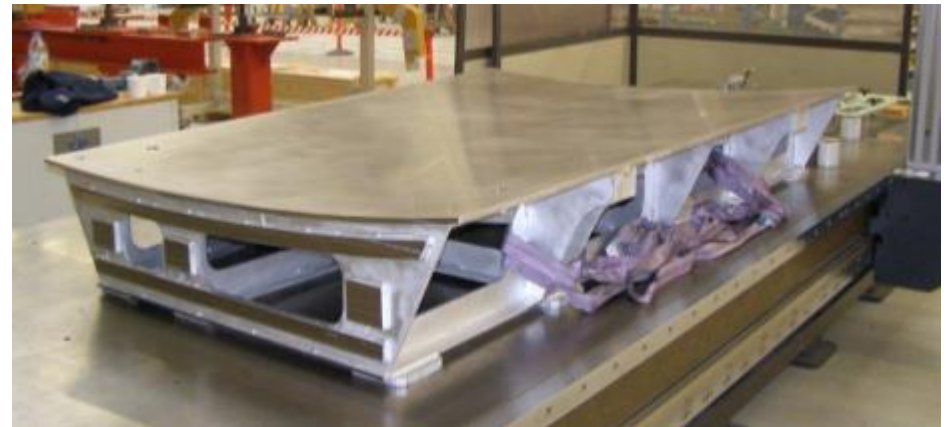
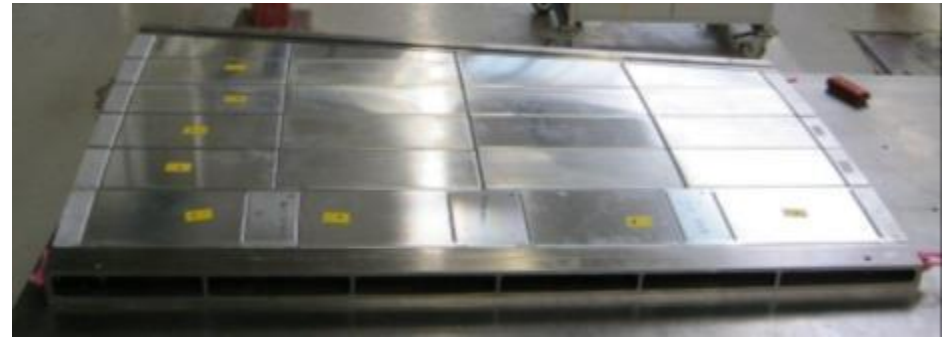
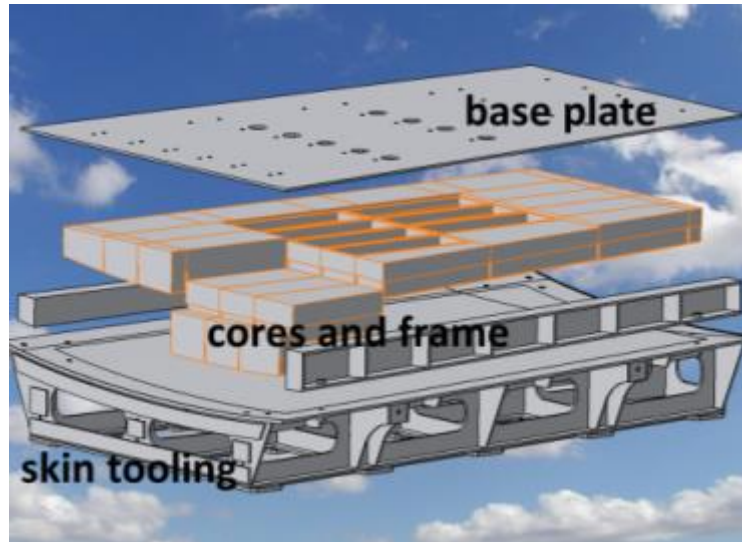
# Manufacturing of Wing Upper Cover



**„CFK-Nord“ – Research Facility  
Stade, Germany**

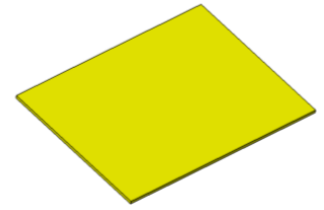


# Cellular Tooling- Validator (36 cores including 10 hollow cores)

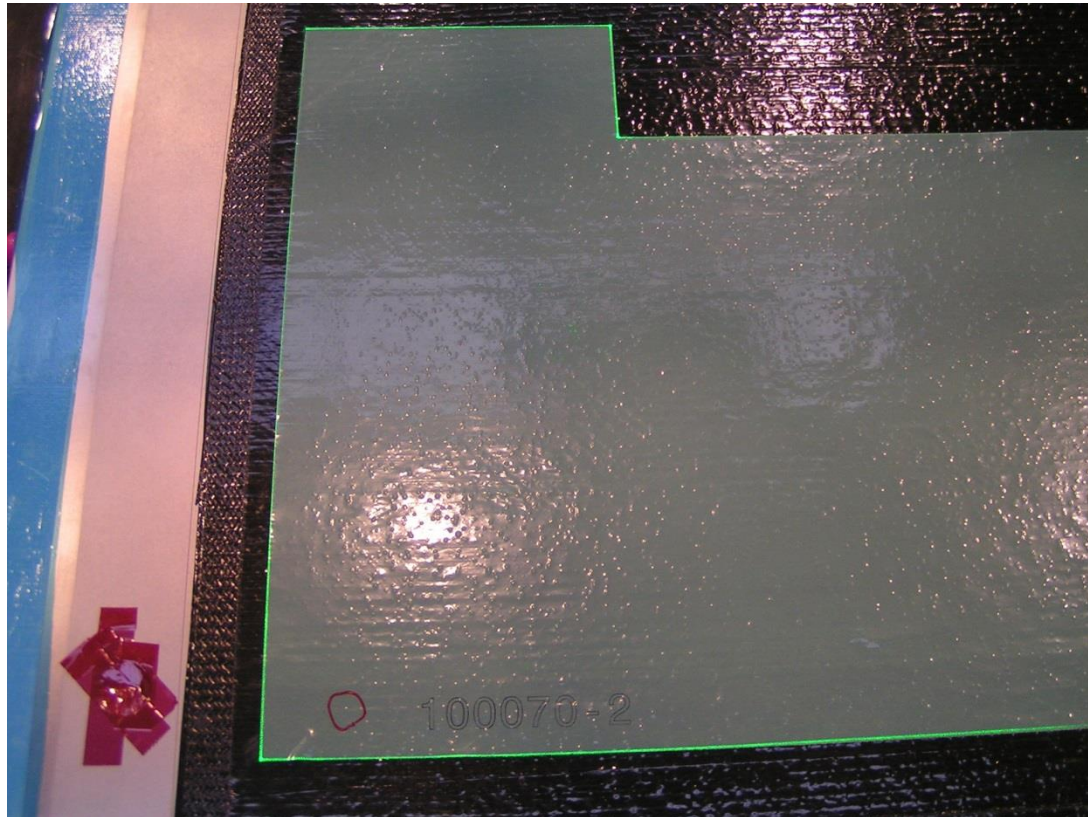
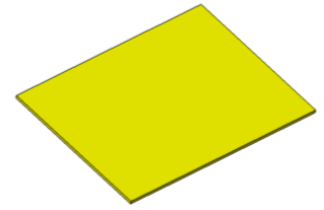




# Skin Plies Layup

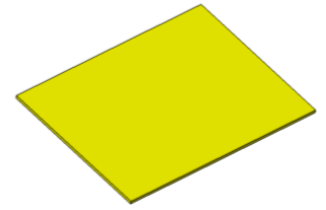


# Skin Plies Layup

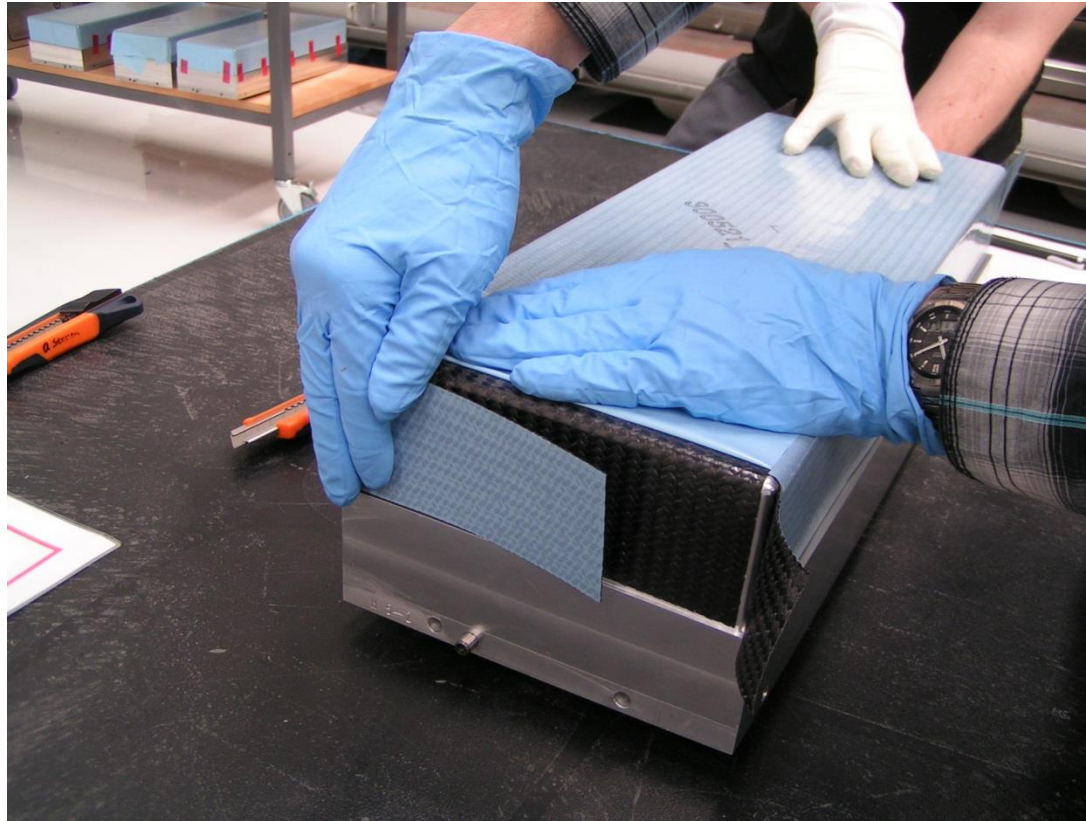
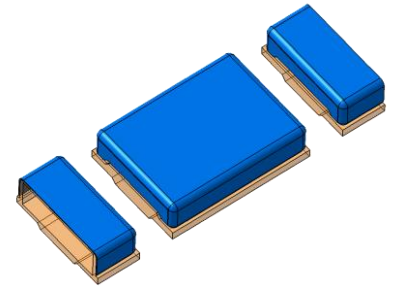




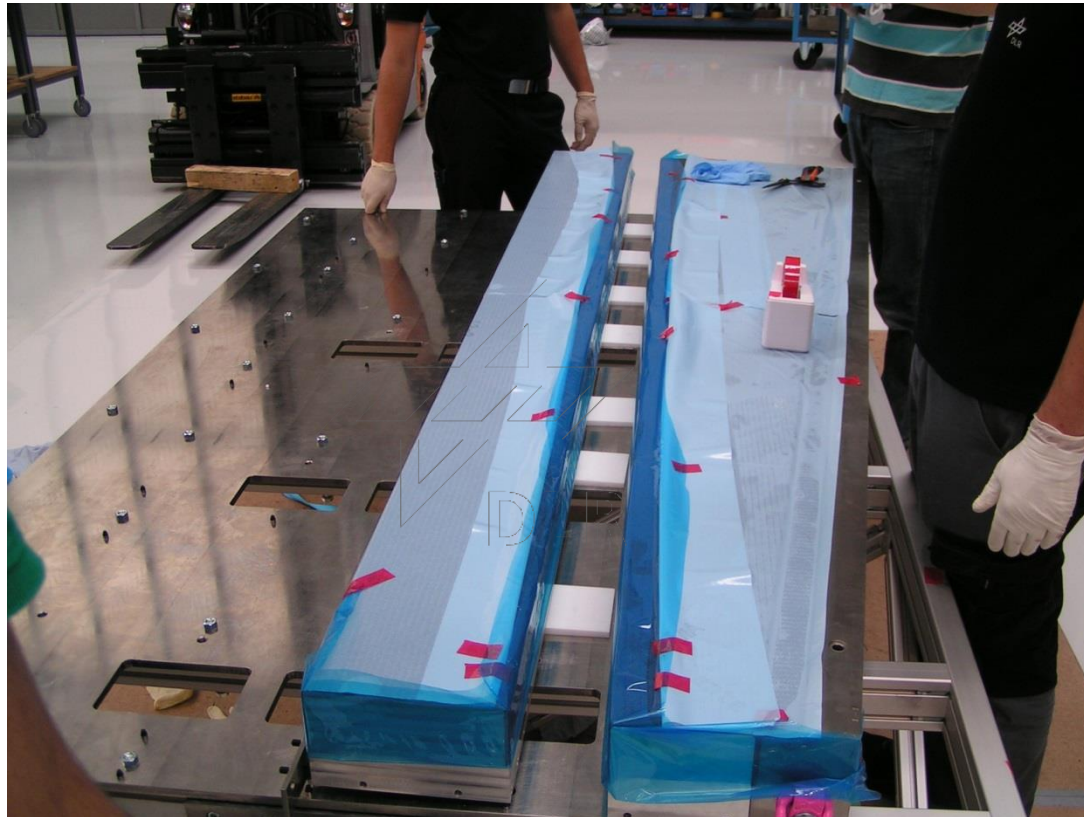
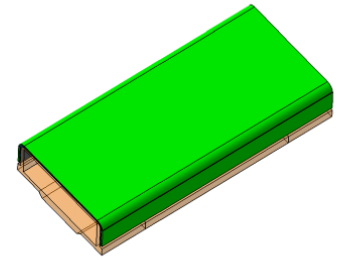
# Skin Plies Consolidation



# Draping Core Plies

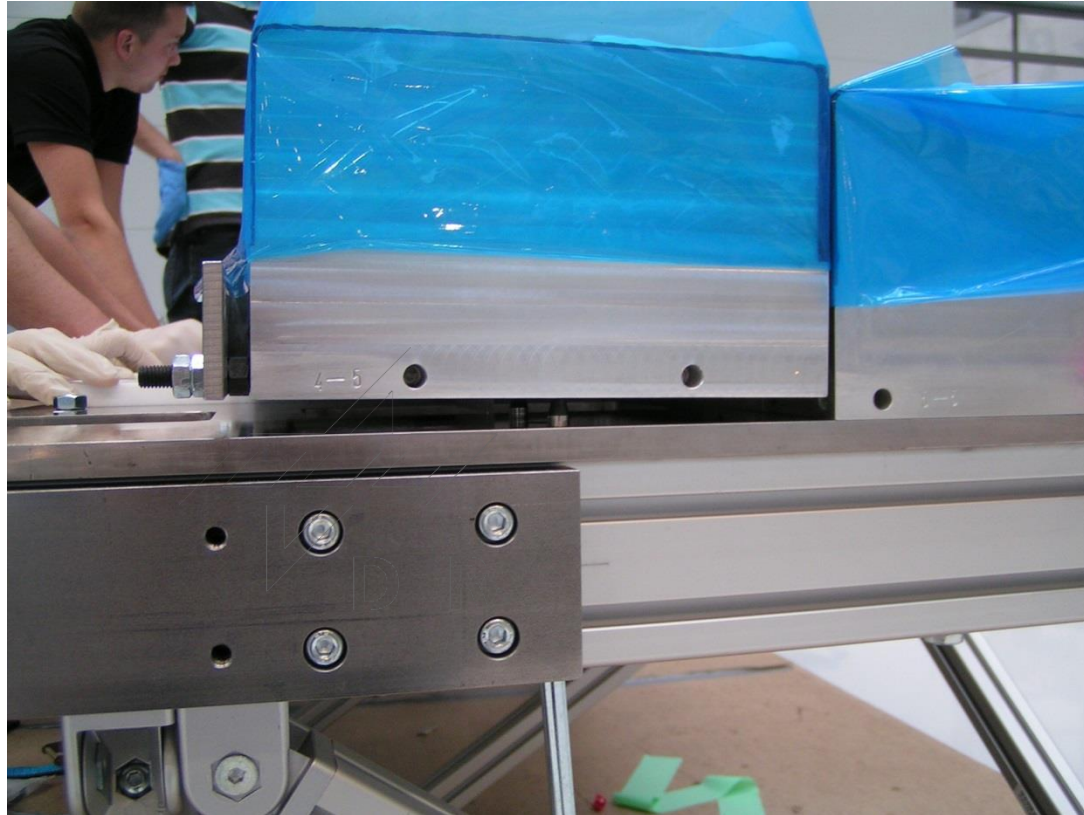
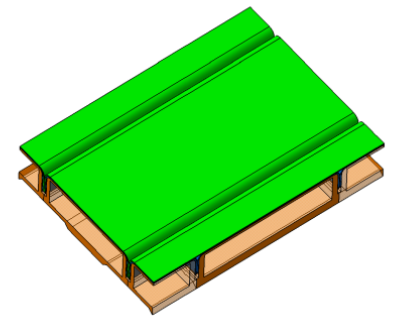


# Positioning of Stringer-Rows

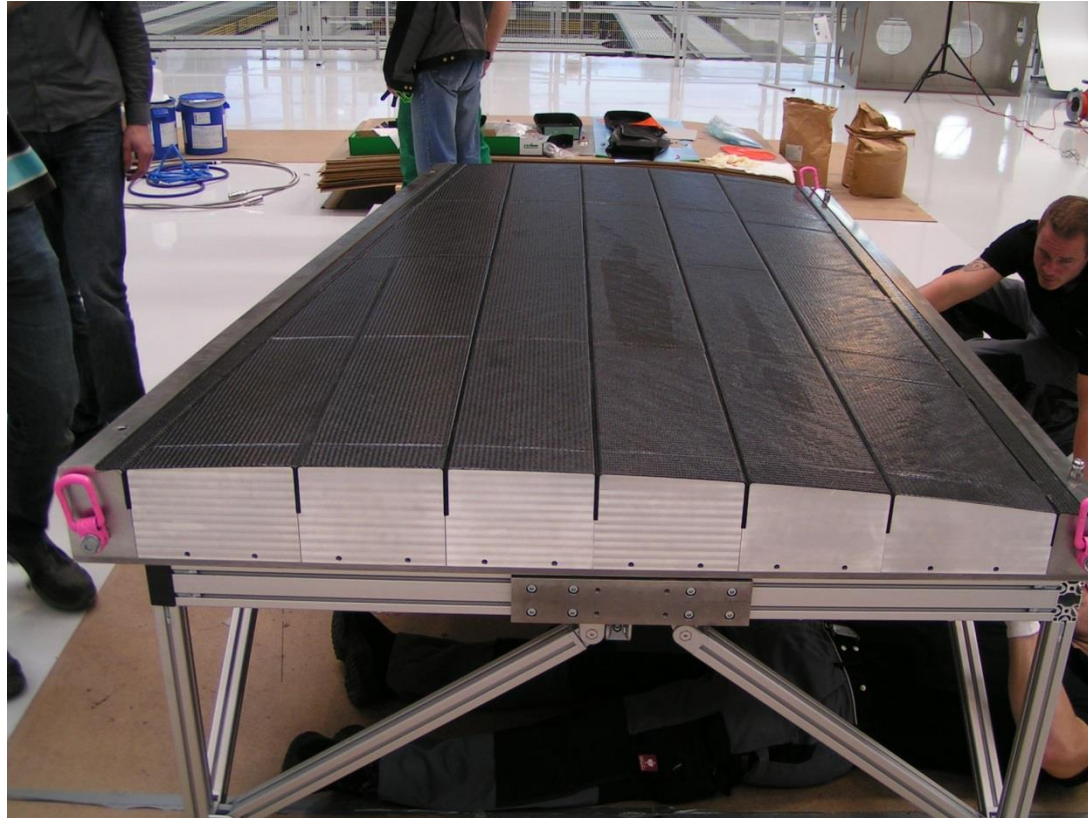
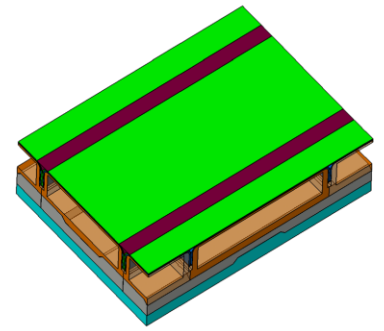




# Positioning of Stringer-Rows

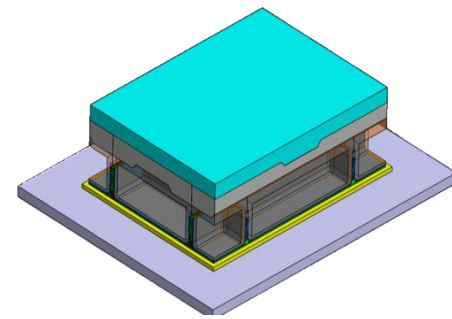


# Integral stiffening Structure

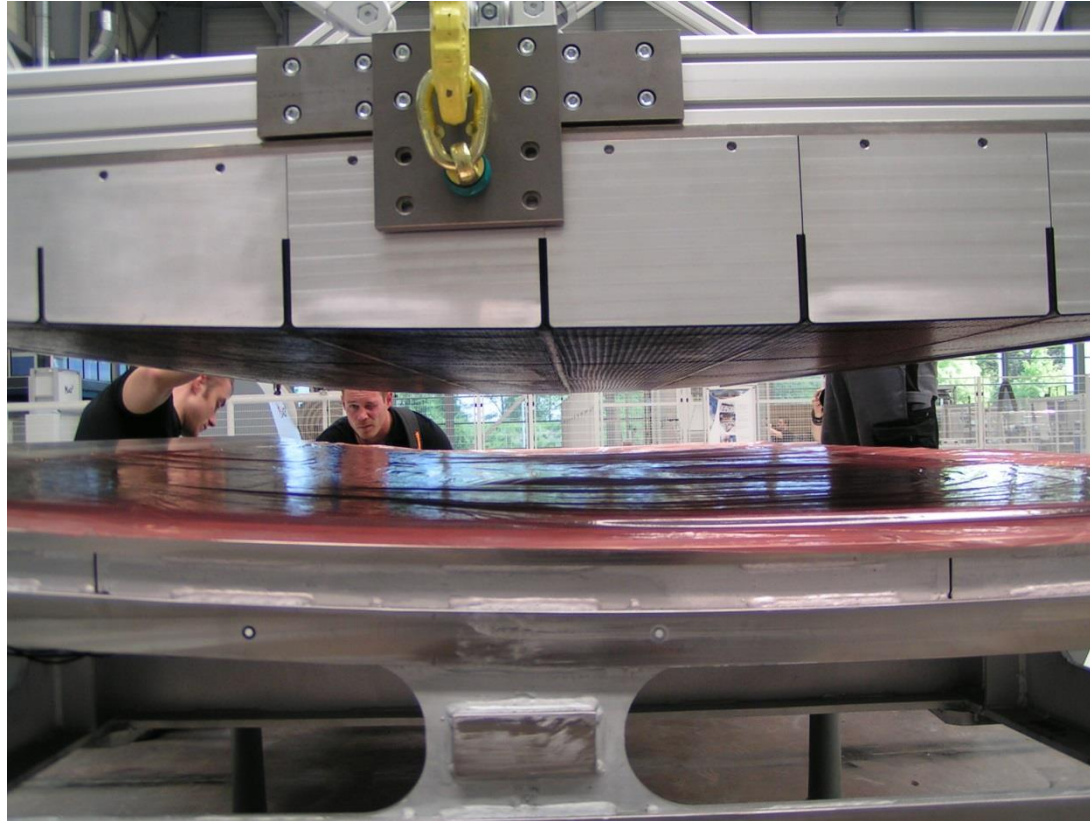
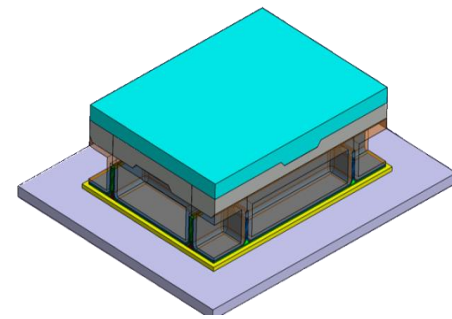




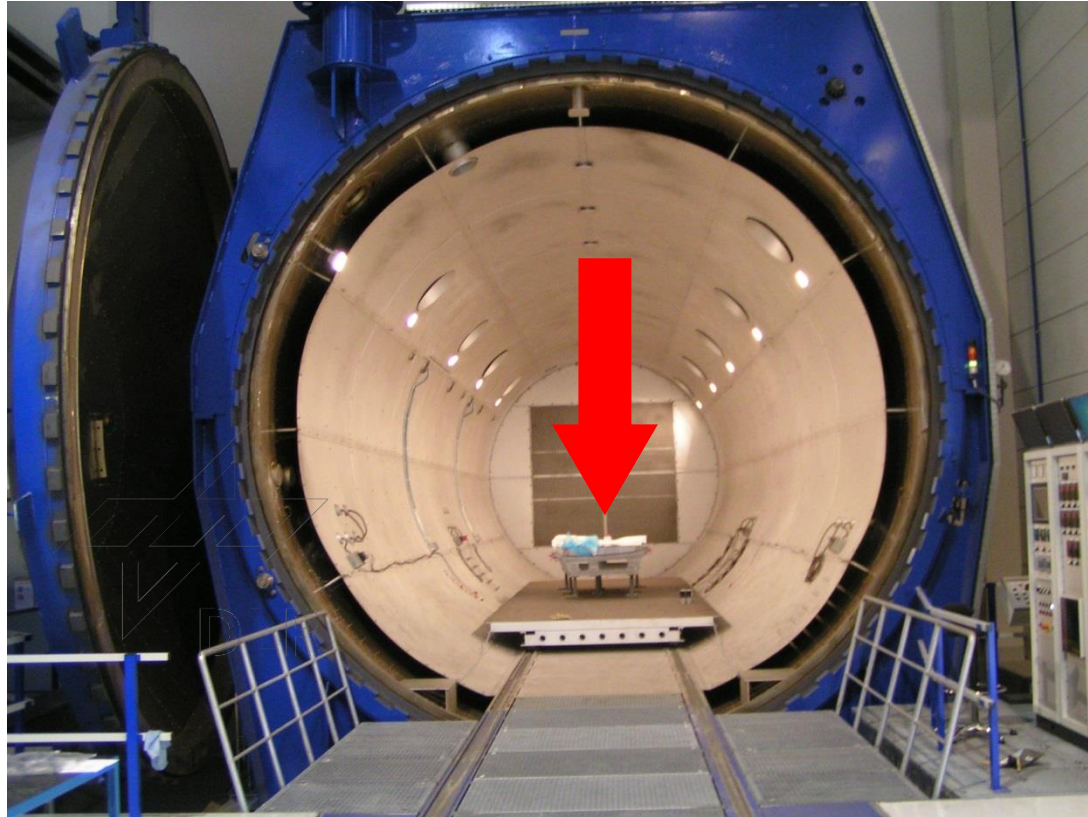
# Unite Skin and Core



# Closing the Tool

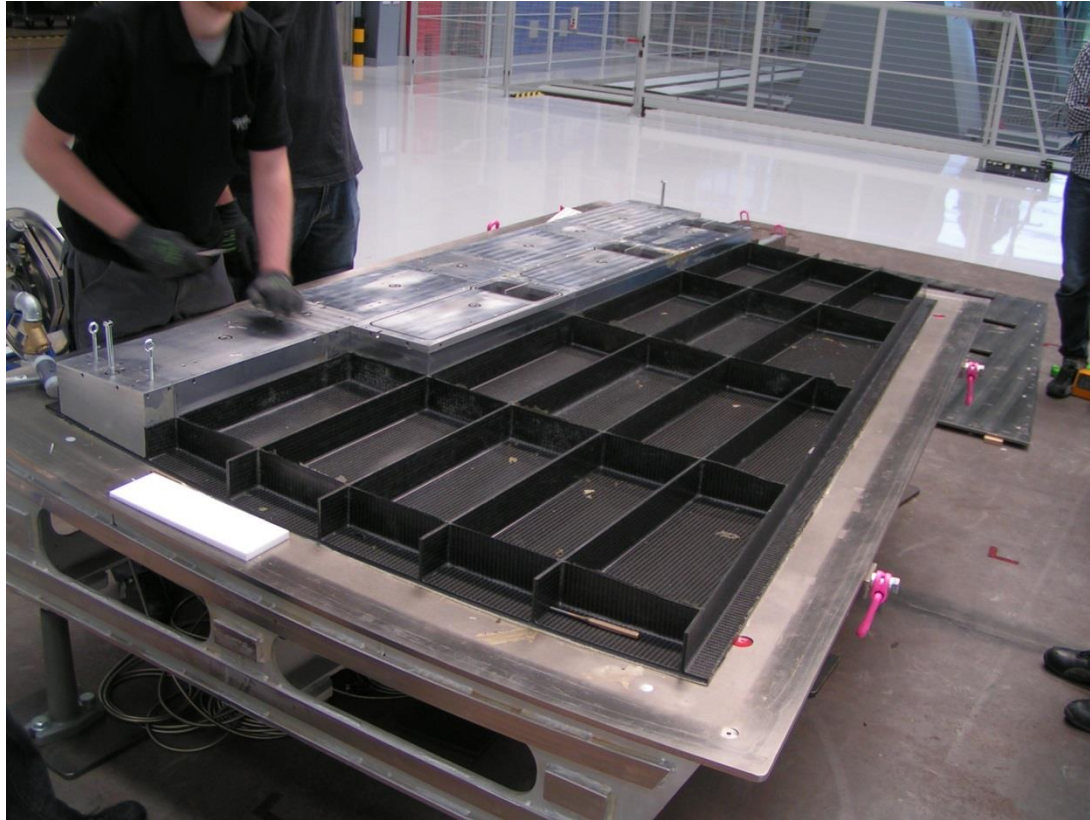


# Autoclave Preparation

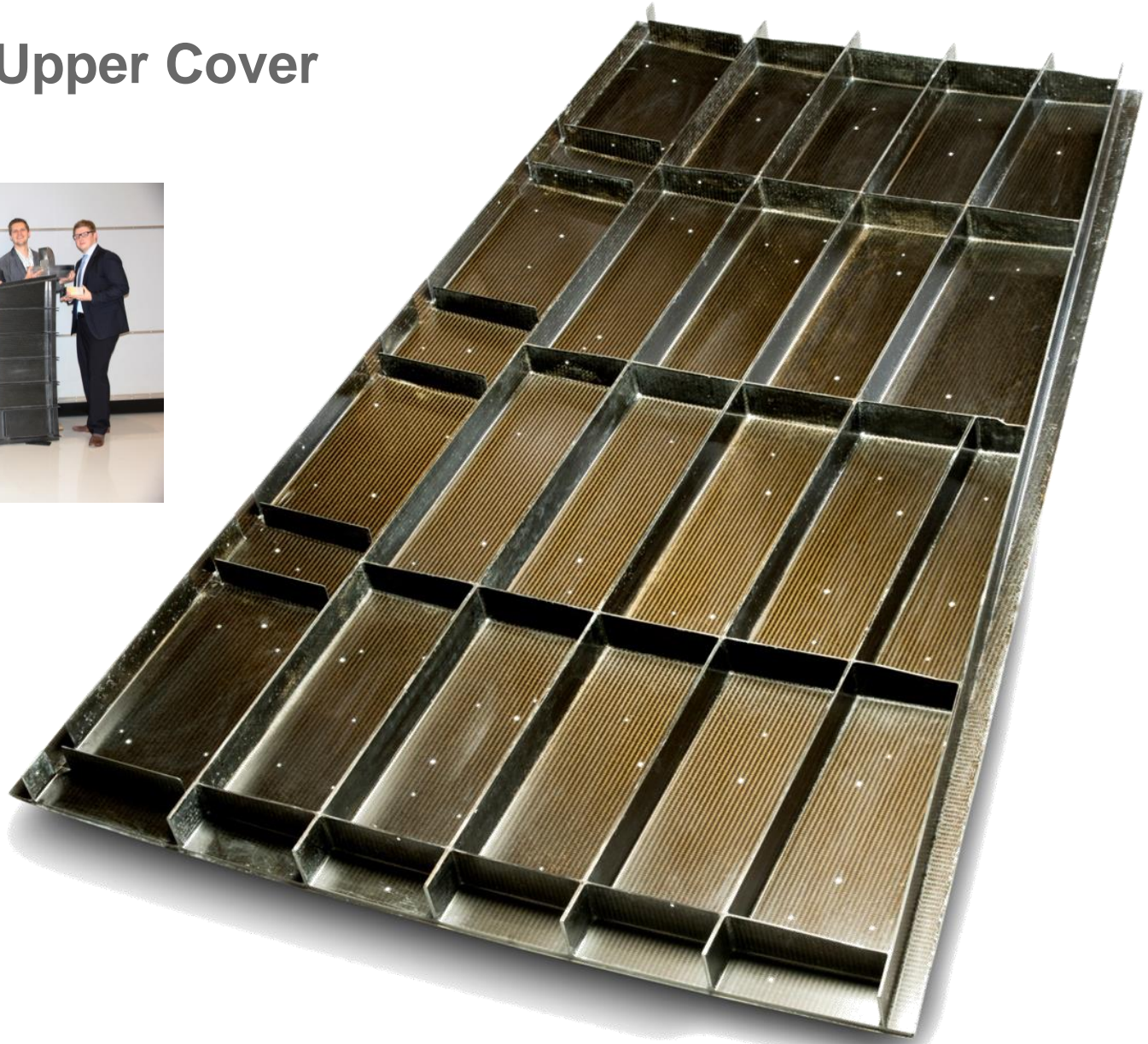




# Demoulding



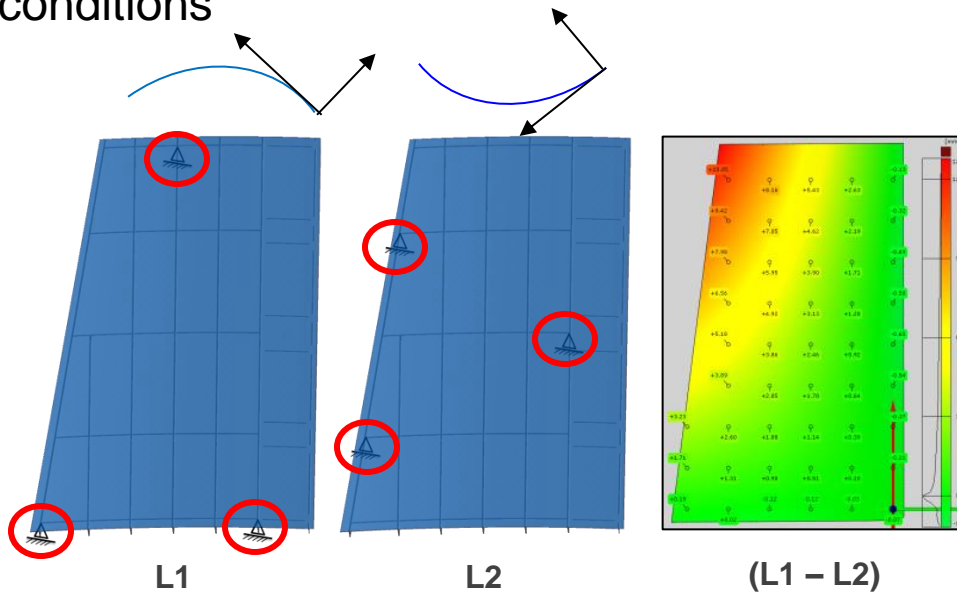
# Wing Upper Cover



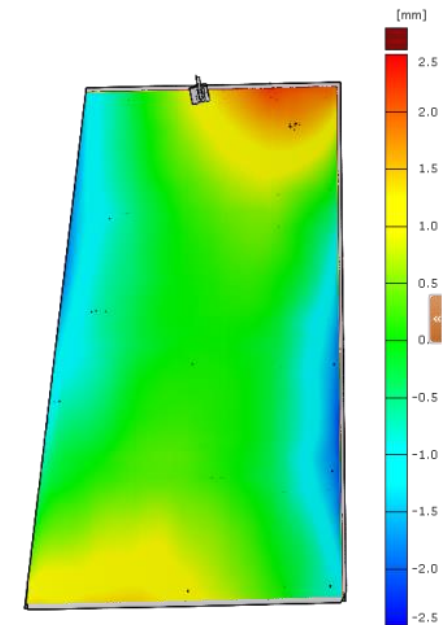


# Waviness Measurement

- Optical 3D-Measurement using gom ATOS
- Best-fit with CAD-model shows global deformation
- Significant influence of gravity with different support conditions

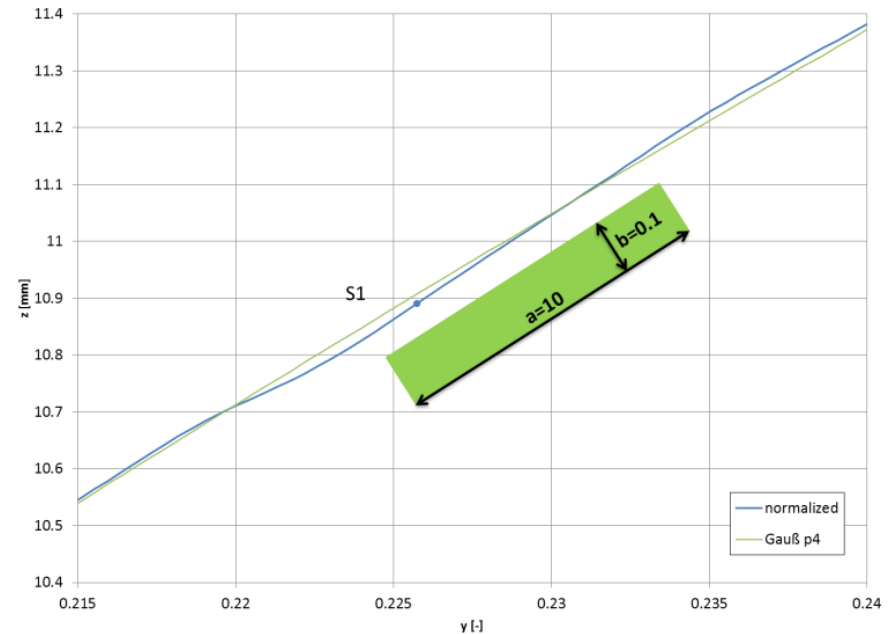


Comparison of different horizontal support conditions



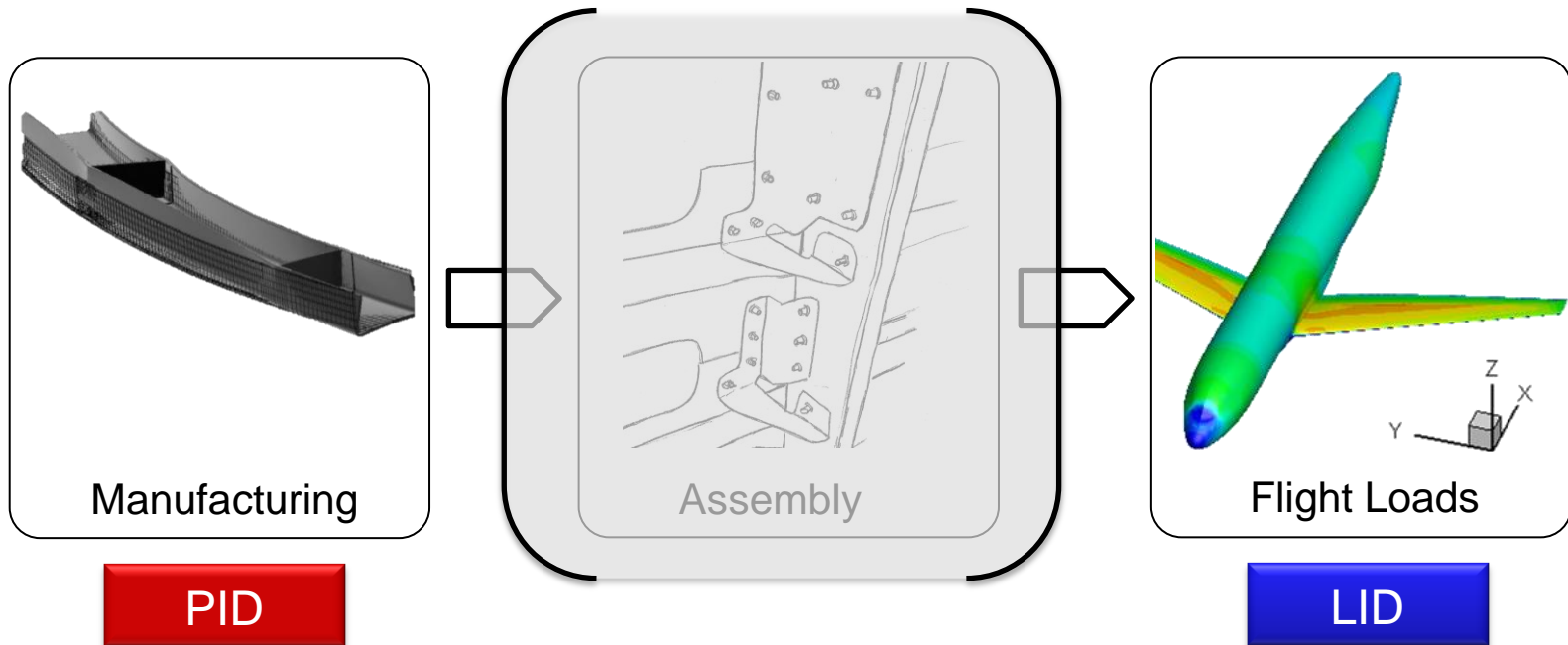
# Waviness Measurement

- Analysis of cross-sections
- Small waves below stringers due to insufficient gusset filler geometry



Gusset-filler waviness

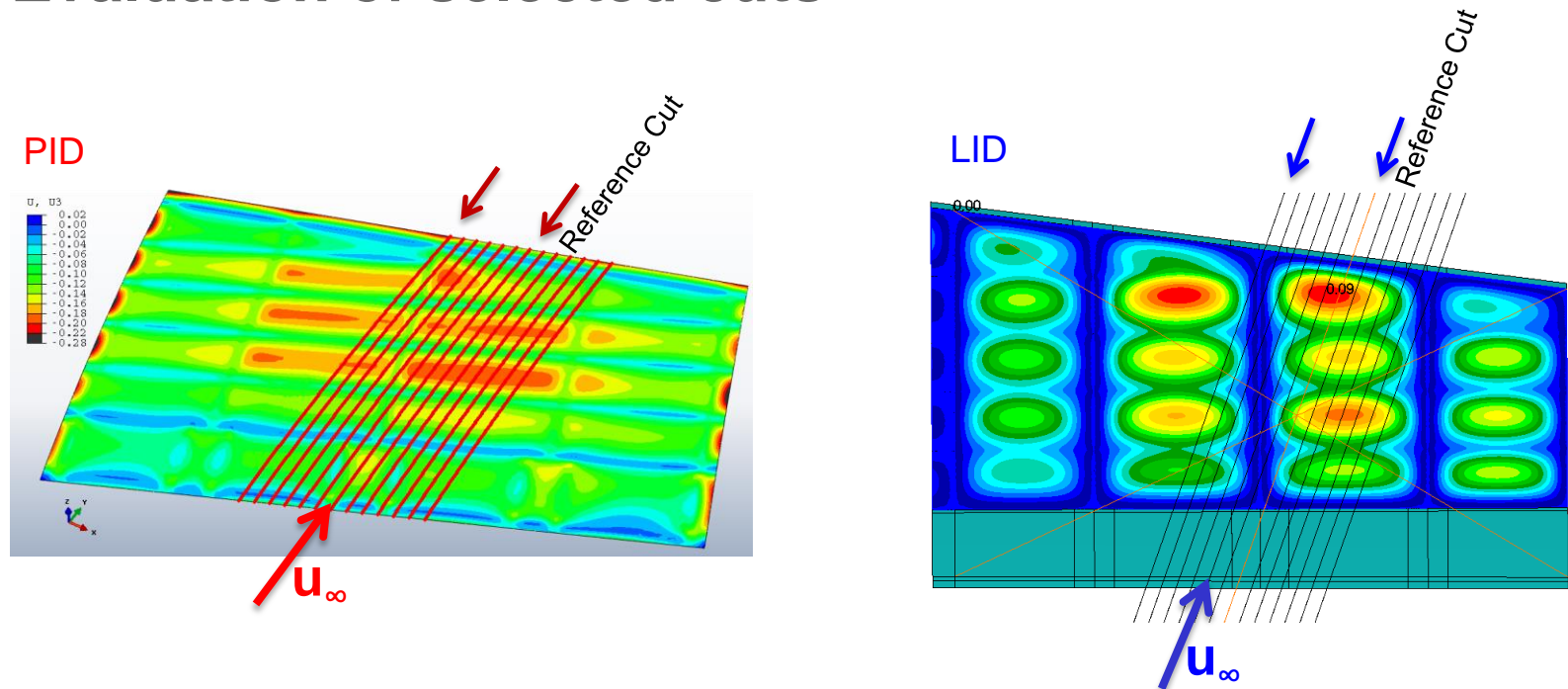
# Resulting Waviness



- Outer shape during cruise flight has deformations due to manufacturing, assembly and aerodynamic loads
- The real part requires an assembly rig
- Simulation substitutes it by adequate BCs



# Evaluation of selected cuts



- Ribs are NOT oriented in flight direction, but perpendicular to front spar
- Two cuts with different characteristics have been selected for more detailed analysis
- Aerodynamic assessment with „2 ½ D“ computational fluid dynamics





# Summary of main Results

Development of integral wing design

- No rivets on aerodynamic surface
- Reduced waviness

Development of cellular tooling concept

- Tolerance management
- Efficient heat-up and cooling

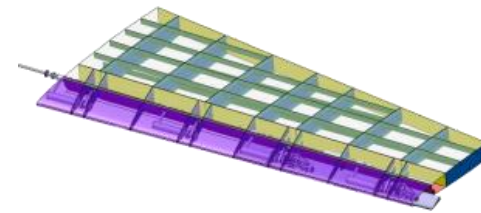
Method for Process induced deformations analysis

- PID-analysis capable for complex stiffened structures

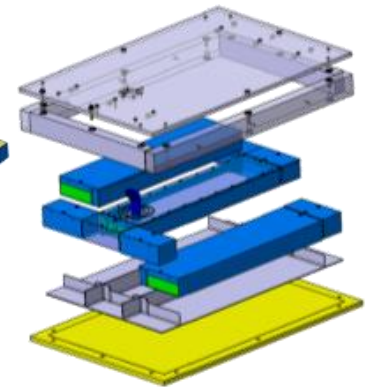
Surface Measurements on validation structures

Manufacturing of full-scale wing cover section

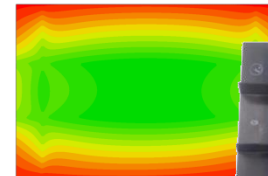
Assessment of resulting waviness from process- & load-induced deformations



Integral wing



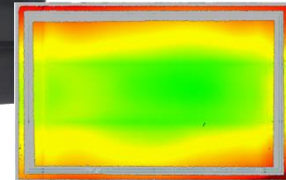
Cellular tooling



PID-Simulation



Manufactured part



Measurement



Move.On LaWO



# Many thanks to our colleagues & partners from

- DLR Institute of Composite Structures and Adaptive Systems, Braunschweig & Stade
- Airbus, Bremen and Filton
- Composite Technology Center, Stade
- Premium Aerotec, Varel
- gom, Gesellschaft für optische Messtechnik, Braunschweig
- BMWi, Federal Ministry for Economic Affairs and Energy



Gefördert durch:



aufgrund eines Beschlusses  
des Deutschen Bundestages



**Tack så mycket!**

**Christian Ückert**

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Knowledge for Tomorrow

